CHAPTER 1

SYSTEMS AND REPRESENTATION

1.1 CONTROL SYSTEM

Control system theory evolved as an engineering discipline and due to universality of the principles involved, it is extended to various fields like economy, sociology, biology, medicine, etc. Control theory has played a vital role in the advance of engineering and science. The automatic control has become an integral part of modern manufacturing and industrial processes. For example, numerical control of machine tools in manufacturing industries, controlling pressure, temperature, humidity, viscosity and flow in process industry.

When a number of elements or components are connected in a sequence to perform a specific function, the group thus formed is called a *system*. In a system when the output quantity is controlled by varying the input quantity, the system is called *control system*. The output quantity is called controlled variable or response and input quantity is called command signal or excitation.

1.2 BASIC ELEMENTS IN CONTROL SYSTEMS

The basic elements of an automatic control system are Error detector, Amplifier and Controller, Actuator (Power actuator), Plant and Sensor or Feedback system. The block diagram of an automatic control system is shown in fig 1.1.

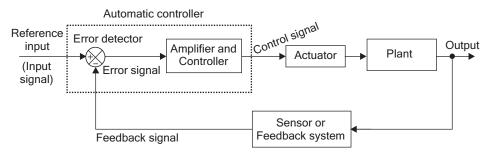


Fig 1.1: Block diagram of control system.

The plant is the open loop system whose output is automatically controlled by closed loop system. The combined unit of error detector, amplifier and controller is called *automatic controller*, because without this unit the system becomes open loop system.

In automatic control systems the reference input will be an input signal proportional to desired output. The feedback signal is a signal proportional to current output of the system. The error detector compares the reference input and feedback signal and if there is a difference it produces an error signal. An amplifier can be used to amplify the error signal and the controller modifies the error signal for better control action.

The actuator amplifies the controller output and converts to the required form of energy that is acceptable for the plant. Depending on the input to the plant, the output will change. This process continues as long as there is a difference between reference input and feedback signal. If the difference is zero, then there is no error signal and the output settles at the desired value.

1. 2 Control Systems

Generally, the error signal will be a weak signal and so it has to be amplified and then modified for better control action. In most of the system the controller itself amplifies the error signal and integrates or differentiates to produce a control signal (i.e., modified error signal). The different types of controllers are P, PI, PD and PID controllers.

1.3 OPEN AND CLOSED LOOP SYSTEMS

OPEN LOOP SYSTEM

Any physical system which does not automatically correct the variation in its output, is called an *open loop system*, or control system in which the output quantity has no effect upon the input quantity are called open-loop control system. This means that the output is not fedback to the input for correction.

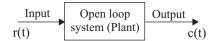


Fig 1.2: Open loop system.

In open loop system the output can be varied by varying the input. But due to external disturbances the system output may change. When the output changes due to disturbances, it is not followed by changes in input to correct the output. In open loop systems the changes in output are corrected by changing the input manually.

CLOSED LOOP SYSTEM

Control systems in which the output has an effect upon the input quantity in order to maintain the desired output value are called *closed loop systems*.

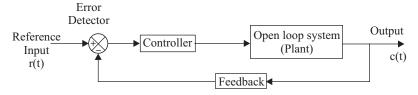


Fig 1.3: Closed loop system.

The open loop system can be modified as closed loop system by providing a feedback. The provision of feedback automatically corrects the changes in output due to disturbances. Hence the closed loop system is also called *automatic control system*. The general block diagram of an automatic control system is shown in fig 1.3. It consists of an error detector, a controller, plant (open loop system) and feedback path elements.

The reference signal (or input signal) corresponds to desired output. The feedback path elements samples the output and converts it to a signal of same type as that of reference signal. The feedback signal is proportional to output signal and it is fed to the error detector. The error signal generated by the error detector is the difference between reference signal and feedback signal. The controller modifies and amplifies the error signal to produce better control action. The modified error signal is fed to the plant to correct its output.

Advantages of open loop systems

- 1. The open loop systems are simple and economical.
- 2. The open loop systems are easier to construct.
- 3. Generally the open loop systems are stable.

Disadvantages of open loop systems

- 1. The open loop systems are inaccurate and unreliable.
- 2. The changes in the output due to external disturbances are not corrected automatically.

Advantages of closed loop systems

- 1. The closed loop systems are accurate.
- 2. The closed loop systems are accurate even in the presence of non-linearities.
- 3. The sensitivity of the systems may be made small to make the system more stable.
- 4. The closed loop systems are less affected by noise.

Disadvantages of closed loop systems

- 1. The closed loop systems are complex and costly.
- 2. The feedback in closed loop system may lead to oscillatory response.
- 3. The feedback reduces the overall gain of the system.
- 4. Stability is a major problem in closed loop system and more care is needed to design a stable closed loop system.

1.3.1 EXAMPLES OF CONTROL SYSTEMS

EXAMPLE 1: TEMPERATURE CONTROL SYSTEM

OPEN LOOP SYSTEM

The electric furnace shown in fig 1.4. is an open loop system. The output in the system is the desired temperature. The temperature of the system is raised by heat generated by the heating element. The output temperature depends on the time during which the supply to heater remains ON.

The ON and OFF of the supply is governed by the time setting of the relay. The temperature is measured by a sensor, which gives an analog voltage corresponding to the temperature of the furnace. The analog signal is converted to digital signal by an Analog - to - Digital converter (A/D converter).

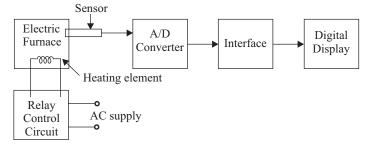


Fig 1.4: Open loop temperature control system.

The digital signal is given to the digital display device to display the temperature. In this system if there is any change in output temperature then the time setting of the relay is not altered automatically.

Control Systems 1.4

CLOSED LOOP SYSTEM

The electric furnace shown in fig 1.5 is a closed loop system. The output of the system is the desired temperature and it depends on the time during which the supply to heater remains ON.

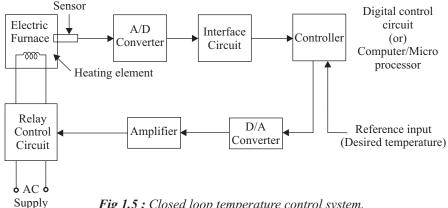


Fig 1.5: Closed loop temperature control system.

The switching ON and OFF of the relay is controlled by a controller which is a digital system or computer. The desired temperature is input to the system through keyboard or as a signal corresponding to desired temperature via ports. The actual temperature is sensed by sensor and converted to digital signal by the A/D converter. The computer reads the actual temperature and compares with desired temperature. If it finds any difference then it sends signal to switch ON or OFF the relay through D/A converter and amplifier. Thus the system automatically corrects any changes in output. Hence it is a closed loop system.

EXAMPLE 2: TRAFFIC CONTROL SYSTEM

OPEN LOOP SYSTEM

Traffic control by means of traffic signals operated on a time basis constitutes an open-loop control system. The sequence of control signals are based on a time slot given for each signal. The time slots are decided based on a traffic study. The system will not measure the density of the traffic before giving the signals. Since the time slot does not changes according to traffic density, the system is open loop system.

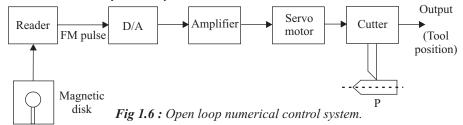
CLOSED LOOP SYSTEM

Traffic control system can be made as a closed loop system if the time slots of the signals are decided based on the density of traffic. In closed loop traffic control system, the density of the traffic is measured on all the sides and the information is fed to a computer. The timings of the control signals are decided by the computer based on the density of traffic. Since the closed loop system dynamically changes the timings, the flow of vehicles will be better than open loop system.

EXAMPLE 3: NUMERICAL CONTROL SYSTEM

OPEN LOOP SYSTEM

Numerical control is a method of controlling the motion of machine components using numbers. Here, the position of work head tool is controlled by the binary information contained in a disk.



A magnetic disk is prepared in binary form representing the desired part P (P is the metal part to be machined). The tool will operate on the desired part P. To start the system, the disk is fed through the reader to the D/A converter. The D/A converter converts the FM(frequency modulated) output of the reader to a analog signal. It is amplified and fed to servometer which positions the cutter on the desired part P. The position of the cutter head is controlled by the angular motion of the servometer. This is an open loop system since no feedback path exists between the output and input. The system positions the tool for a given input command. Any deviation in the desired position is not checked and corrected automatically.

CLOSED LOOP SYSTEM

A magnetic disk is prepared in binary form representing the desired part P (P is the metal part to be machined). To start the system, the disk is loaded in the reader. The controller compares the frequency modulated input pulse signal with the feedback pulse signal. The controller is a computer or microprocessor system. The controller carries out mathematical operations on the difference in the pulse signals and generates an error signal. The D/A converter converts the controller output pulse (error signal) into an analog signal. The amplified analog signal rotates the servomotor to position the tool on the job. The position of the cutterhead is controlled according to the input of the servomotor.

The transducer attached to the cutterhead converts the motion into an electrical signal. The analog electrical signal is converted to the digital pulse signal by the A/D converter. Then this signal is compared with the input pulse signal. If there is any difference between these two, the controller sends a signal to the servomotor to reduce it. Thus the system automatically corrects any deviation in the desired output tool position. An advantage of numerical control is that complex parts can be produced with uniform tolerances at the maximum milling speed.

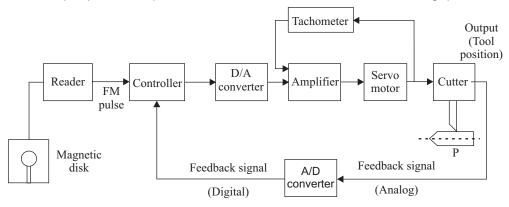


Fig 1.7: Closed loop numerical control system.

EXAMPLE 4: POSITION CONTROL SYSTEM USING SERVOMOTOR

The position control system shown in fig 1.8 is a closed loop system. The system consists of a servomotor powered by a generator. The load whose position has to be controlled is connected to motor shaft through gear wheels. Potentiometers are used to convert the mechanical motion to electrical signals. The desired load position (θ_R) is set on the input potentiometer and the actual load position (θ_C) is fed to feedback potentiometer. The difference between the two angular positions generates an error signal, which is amplified and fed to generator field circuit. The induced emf of the generator drives the motor. The rotation of the motor stops when the error signal is zero, i.e. when the desired load position is reached.

This type of control systems are called servomechanisms. The **servo** or **servomechanisms** are feedback control systems in which the output is mechanical position (or time derivatives of position e.g. velocity and acceleration).

1. 6 Control Systems

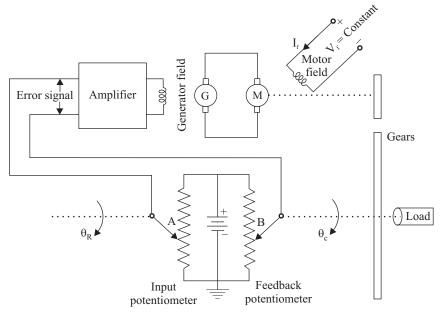


Fig 1.8: A position control system (servomechanism).

1.4 MATHEMATICAL MODELS OF CONTROL SYSTEMS

A *control system* is a collection of physical objects (components) connected together to serve an objective. The input output relations of various physical components of a system are governed by *differential equations*. The mathematical model of a control system constitutes a set of differential equations. The response or output of the system can be studied by solving the differential equations for various input conditions.

The mathematical model of a system is linear if it obeys the principle of superposition and homogenity. This principle implies that if a system model has responses $y_1(t)$ and $y_2(t)$ to any inputs $x_1(t)$ and $x_2(t)$ respectively, then the system response to the linear combination of these inputs $a_1x_1(t) + a_2x_2(t)$ is given by linear combination of the individual outputs $a_1y_1(t) + a_2y_2(t)$, where a_1 and a_2 are constants.

The principle of superposition can be explained diagrammatically as shown in fig. 1.9.

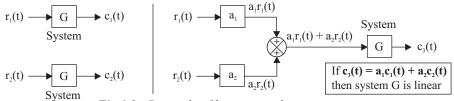


Fig 1.9: Principle of linearity and superposition.

A mathematical model will be linear if the differential equations describing the system has constant coefficients (or the coefficients may be functions of independent variables). If the coefficients of the differential equation describing the system are constants then the model is *linear time invariant*. If the coefficients of differential equations governing the system are functions of time then the model is *linear time varying*.

1.5 MECHANICAL TRANSLATIONAL SYSTEMS

The model of mechanical translational systems can be obtained by using three basic elements *mass*, *spring and dash-pot*. These three elements represents three essential phenomena which occur in various ways in mechanical systems.

The weight of the mechanical system is represented by the element *mass* and it is assumed to be concentrated at the center of the body. The elastic deformation of the body can be represented by a *spring*. The friction existing in rotating mechanical system can be represented by the *dash-pot*. The dash-pot is a piston moving inside a cylinder filled with viscous fluid.

When a force is applied to a translational mechanical system, it is opposed by opposing forces due to mass, friction and elasticity of the system. The force acting on a mechanical body are governed by *Newton's second law of motion*. For translational systems it states that the sum of forces acting on a body is zero. (or Newton's second law states that the sum of applied forces is equal to the sum of opposing forces on a body).

LIST OF SYMBOLS USED IN MECHANICAL TRANSLATIONAL SYSTEM

x = Displacement, m

$$v = \frac{dx}{dt}$$
 = Velocity, m/sec

$$a = \frac{dv}{dt} = \frac{d^2x}{dt^2} = Acceleration, m/sec^2$$

f = Applied force, N (Newtons)

f_m = Opposing force offered by mass of the body, N

 f_k = Opposing force offered by the elasticity of the body (spring), N

 f_b = Opposing force offered by the friction of the body (dash - pot), N

M = Mass, kg

K = Stiffness of spring, N/m

B = Viscous friction co-efficient, N-sec/m

 $\it Note: Lower\ case\ letters\ are\ functions\ of\ time.$

FORCE BALANCE EQUATIONS OF IDEALIZED ELEMENTS

Consider an ideal mass element shown in fig 1.10 which has negligible friction and elasticity. Let a force be applied on it. The mass will offer an opposing force which is proportional to acceleration of the body.

Let,
$$f = Applied$$
 force
 $f_m = Opposing$ force due to mass
Here, $f_m \propto \frac{d^2x}{dt^2}$ or $f_m = M\frac{d^2x}{dt^2}$

By Newton's second law,
$$f = f_m = M \frac{d^2x}{dt^2}$$
(1.1)

Fig 1.10: Ideal mass element.

Consider an ideal frictional element dashpot shown in fig 1.11 which has negligible mass and elasticity. Let a force be applied on it. The dash-pot will offer an opposing force which is proportional to velocity of the body.

1. 8 Control Systems

Let, f = Applied force

 $f_b = Opposing force due to friction$

Here,
$$f_b \propto \frac{dx}{dt}$$
 or $f_b = B \frac{dx}{dt}$

By Newton's second law,
$$f = f_b = B \frac{dx}{dt}$$
(1.2)

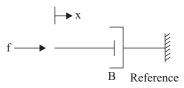


Fig 1.11: Ideal dashpot with one end fixed to reference.

When the dashpot has displacement at both ends as shown in fig 1.12, the opposing force is proportional to difference between velocity at both ends.

$$\begin{split} f_b & \propto \frac{d}{dt}(x_1 - x_2) \quad \text{ or } \quad f_b = B \, \frac{d}{dt}(x_1 - x_2) \\ & \therefore \left[f = f_b = B \, \frac{d}{dt}(x_1 - x_2) \right] \qquad \qquad(1.3) \end{split}$$

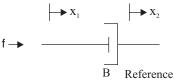


Fig 1.12: Ideal dashpot with displacement at both ends.

Consider an ideal elastic element spring shown in fig 1.13, which has negligible mass and friction. Let a force be applied on it. The spring will offer an opposing force which is proportional to displacement of the body.

Let, f = Applied force $f_k = Opposing$ force due to elasticity

Here $f_{\nu} \propto x$ or $f_{\nu} = K x$

By Newton's second law,
$$f = f_k = Kx$$
(1.4)

 $f \longrightarrow X$ $f \longrightarrow K$ Reference

Fig 1.13: Ideal spring with one end fixed to reference.

When the spring has displacement at both ends as shown in fig 1.14 the opposing force is proportional to difference between displacement at both ends.

$$f_k \propto (x_1 - x_2)$$
 or $f_k = K(x_1 - x_2)$
 $\therefore f = f_k = K(x_1 - x_2)$ (1.5)

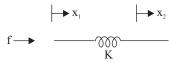


Fig 1.14: Ideal spring with displacement at both ends.

Guidelines to determine the Transfer Function of Mechanical Translational System

- In mechanical translational system, the differential equations governing the system are
 obtained by writing force balance equations at nodes in the system. The nodes are meeting
 point of elements. Generally the nodes are mass elements in the system. In some cases the
 nodes may be without mass element.
- 2. The linear displacement of the masses (nodes) are assumed as x_1 , x_2 , x_3 , etc., and assign a displacement to each mass(node). The first derivative of the displacement is velocity and the second derivative of the displacement is acceleration.
- 3. Draw the free body diagrams of the system. The free body diagram is obtained by drawing each mass separately and then marking all the forces acting on that mass (node). Always the opposing force acts in a direction opposite to applied force. The mass has to move in the direction of the applied force. Hence the displacement, velocity and acceleration of the mass will be in the direction of the applied force. If there is no applied force then the

displacement, velocity and acceleration of the mass will be in a direction opposite to that of opposing force.

- 4. For each free body diagram, write one differential equation by equating the sum of applied forces to the sum of opposing forces.
- 5. Take Laplace transform of differential equations to convert them to algebraic equations. Then rearrange the s-domain equations to eliminate the unwanted variables and obtain the ratio between output variable and input variable. This ratio is the transfer function of the system.

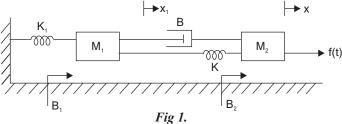
Note: Laplace transform of
$$x(t) = \mathcal{L}\{x(t)\} = X(s)$$

$$Laplace \ transform \ of \ \frac{dx(t)}{dt} = \mathcal{L}\left\{\frac{d}{dt}x(t)\right\} = s \ X(s) \ (with \ zero \ initial \ conditions)$$

$$Laplace \ transform \ of \ \frac{d^2x(t)}{dt^2} = \mathcal{L}\left\{\frac{d^2}{dt^2}x(t)\right\} = s^2 \ X(s) \ (with \ zero \ initial \ conditions)$$

EXAMPLE 1.1

Write the differential equations governing the mechanical system shown in fig 1. and determine the transfer function.



SOLUTION

In the given system, applied force 'f(t)' is the input and displacement 'x' is the output.

Let, Laplace transform of $f(t) = \mathcal{L}\{f(t)\} = F(s)$

Laplace transform of $x = \mathcal{L}\{x\} = X(s)$

Laplace transform of $x_1 = \mathcal{L}\{x_1\} = X_1(s)$

Hence the required transfer function is $\frac{X(s)}{F(s)}$

The system has two nodes and they are mass $\rm M_1$ and $\rm M_2$. The differential equations governing the system are given by force balance equations at these nodes.

Let the displacement of mass M_1 be x_1 . The free body diagram of mass M_1 is shown in fig 2. The opposing forces acting on mass M_1 are marked as f_{m1} , f_{b1} , f_{b} , f_{k1} and f_{k} .

$$f_{m1} = M_1 \frac{d^2 x_1}{dt^2}$$
; $f_{b1} = B_1 \frac{dx_1}{dt}$; $f_{k1} = K_1 x_1$;
 $f_b = B \frac{d}{dt} (x_1 - x)$; $f_k = K(x_1 - x)$

By Newton's second law,

$$\begin{split} &f_{m1} + f_{b1} + f_b + f_{k1} + f_k = 0 \\ & \therefore \ M_1 \frac{d^2 x_1}{dt^2} + B_1 \frac{d x_1}{dt} + B \frac{d}{dt} (x_1 - x) + K_1 x_1 + K(x_1 - x) = 0 \end{split}$$

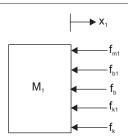


Fig 2: Free body diagram of mass M_1 (node 1).

On taking Laplace transform of above equation with zero initial conditions we get,

$$M_1s^2X_1(s) + B_1sX_1(s) + Bs[X_1(s) - X(s)] + K_1X_1(s) + K[X_1(s) - X(s)] = 0$$

$$X_1(s) [M_1s^2 + (B_1 + B)s + (K_1 + K)] - X(s) [Bs + K] = 0$$

$$X_1(s) [M_1s^2 + (B_1 + B)s + (K_1 + K)] = X(s) [Bs + K]$$

$$\therefore X_1(s) = X(s) = \frac{Bs + K}{M_1 s^2 + (B_1 + B)s + (K_1 + K)}$$
.....(1)

The free body diagram of mass M_2 is shown in fig 3. The opposing forces acting on M_2 are marked as f_{m2} , f_{b2} , f_b and f_b .

$$f_{m2} = M_2 \frac{d^2x}{dt^2}$$
 ; $f_{b2} = B_2 \frac{dx}{dt}$

$$f_b = B \frac{d}{dt}(x - x_1)$$
 ; $f_k = K(x - x_1)$

By Newton's second law,

$$f_{m2} + f_{b2} + f_b + f_k = f(t)$$

$$M_2 \frac{d^2x}{dt^2} + B_2 \frac{dx}{dt} + B \frac{d}{dt} (x - x_1) + K(x - x_1) = f(t)$$

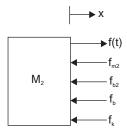


Fig 3: Free body diagram of mass M_2 (node 2).

On taking Laplace transform of above equation with zero initial conditions we get,

$$\mathsf{M}_2 s^2 \mathsf{X}(s) + \mathsf{B}_2 s \mathsf{X}(s) + \mathsf{B} s [\mathsf{X}(s)] - \mathsf{X}_1(s)] + \mathsf{K}[\mathsf{X}(s) - \mathsf{X}_1(s)] = \mathsf{F}(s)$$

$$X(s)[M_2s^2 + (B_2 + B)s + K] - X_1(s)[Bs + K] = F(s)$$
(2)

Substituting for X₁(s) from equation (1) in equation (2) we get,

$$\begin{split} X(s)\left[M_{2}s^{2}+(B_{2}+B)s+K\right]-X(s)\frac{(Bs+K)^{2}}{M_{1}s^{2}+(B_{1}+B)s+(K_{1}+K)}=F(s)\\ X(s)\left[\frac{\left[M_{2}s^{2}+(B_{2}+B)s+K\right]\left[M_{1}s^{2}+(B_{1}+B)s+(K_{1}+K)\right]-(Bs+K)^{2}}{M_{1}s^{2}+(B_{1}+B)s+(K_{1}+K)}\right]=F(s) \end{split}$$

$$\ \, \therefore \ \, \frac{X(s)}{F(s)} = \frac{M_1 s^2 + (B_1 + B) s + (K_1 + K)}{[M_1 s^2 + (B_1 + B) s + (K_1 + K)] - [M_2 s^2 + (B_2 + B) s + K] - (Bs + K)^2}$$

RESULT

The differential equations governing the system are,

1.
$$M_1 \frac{d^2 x_1}{dt^2} + B_1 \frac{d x_1}{dt} + B \frac{d}{dt}(x_1 - x) + K_1 x_1 + K(x_1 - x) = 0$$

2.
$$M_2 \frac{d^2x}{dt^2} + B_2 \frac{dx}{dt} + B \frac{d}{dt} (x - x_1) + K(x - x_1) = f(t)$$

The transfer function of the system is

$$\frac{X(s)}{F(s)} = \frac{M_1 s^2 + (B_1 + B) s + (K_1 + K)}{[M_1 s^2 + (B_1 + B) s + (K_1 + K)][M_2 s^2 + (B_2 + B) s + K] - (Bs + K)^2}$$

EXAMPLE 1.2

Determine the transfer function $\frac{Y_2(s)}{F(s)}$ of the system shown in fig 1.

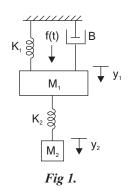
SOLUTION

Let, Laplace transform of $f(t) = \mathcal{L}\{f(t)\} = F(s)$

Laplace transform of $y_1 = \mathcal{L}\{y_1\} = Y_1(s)$

Laplace transform of $y_2 = \mathcal{L}\{y_2\} = Y_2(s)$

The system has two nodes and they are mass $\rm M_1$ and $\rm M_2$. The differential equations governing the system are the force balance equations at these nodes.



The free body diagram of mass M₁ is shown in fig 2.

The opposing forces are marked as f_{m1} , f_{h} , f_{k1} and f_{k2}

$$f_{m1} = M_1 \frac{d^2 y_1}{dt^2}$$
; $f_b = B \frac{dy_1}{dt}$; $f_{k1} = K_1 y_1$; $f_{k2} = K_2 (y_1 - y_2)$

By Newton's second law, $f_{m1} + f_b + f_{k1} + f_{k2} = f(t)$

$$\therefore M_1 \frac{d^2 y_1}{dt^2} + B \frac{d y_1}{dt} + K_1 y_1 + K_2 (y_1 - y_2) = f(t) \qquad(1)$$

On taking Laplace transform of equation (1) with zero initial condition we get,

$$\begin{aligned} &M_1 s^2 Y_1(s) + B s Y_1(s) + K_1 Y_1(s) + K_2 [Y_1(s) - Y_2(s)] = F(s) \\ &Y_1(s) [M_1 s^2 + B s + (K_1 + K_2)] - Y_2(s) K_2 = F(s) \end{aligned} \qquad(2)$$

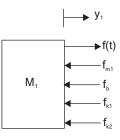


Fig 2.

The free body diagram of mass M_2 is shown in fig 3. The opposing forces acting on M_2 are f_{m2} and f_{k2} .

$$f_{m2} = M_2 \frac{d^2 y_2}{dt^2}$$
 ; $f_{k2} = K_2 (y_2 - y_1)$

By Newton's second law, $f_{m2} + f_{k2} = 0$

$$\therefore M_2 \frac{d^2 y_2}{dt^2} + K_2 (y_2 - y_1) = 0$$

On taking Laplace transform of above equation we get,

$$M_2s^2Y_2(s) + K_2[Y_2(s) - Y_1(s)] = 0$$

$$Y_2(s) [M_2 s^2 + K_2] - Y_1(s) K_2 = 0$$

$$\therefore Y_1(s) = Y_2(s) \frac{M_2 s^2 + K_2}{K_2} \qquad(3)$$

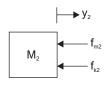


Fig 3.

Substituting for Y₁(s) from equation (3) in equation (2) we get,

$$Y_{2}(s) \left[\frac{M_{2}s^{2} + K_{2}}{K_{2}} \right] [M_{1}s^{2} + Bs + (K_{1} + K_{2})] - Y_{2}(s) K_{2} = F(s)$$

$$Y_{2}(s) \left[\frac{(M_{2}s^{2} + K_{2})[M_{1}s^{2} + Bs + (K_{1} + K_{2})] - K_{2}^{2}}{K_{2}} \right] = F(s)$$

$$\label{eq:final_continuity} \cdot \cdot \cdot \frac{Y_2(s)}{F(s)} = \frac{K_2}{[M_1 s^2 + B s + (K_1 + K_2)][M_2 s^2 + K_2] - K_2^2}$$

RESULT

The differential equations governing the system are,

1.
$$M_1 \frac{d^2 y_1}{dt^2} + B \frac{dy_1}{dt} + K_1 y_1 + K_2 (y_1 - y_2) = f(t)$$

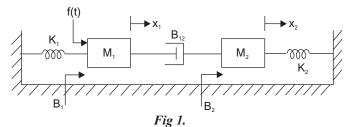
2.
$$M_2 \frac{d^2 y_2}{dt^2} + K_2 (y_2 - y_1) = 0$$

The transfer function of the system is,

$$\frac{Y_2(s)}{F(s)} = \frac{K_2}{[M_1 s^2 + Bs + (K_1 + K_2)][M_2 s^2 + K_2] - K_2^2}$$

EXAMPLE 1.3

Determine the transfer function, $\frac{X_1(s)}{F(s)}$ and $\frac{X_2(s)}{F(s)}$ for the system shown in fig 1.

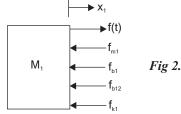


SOLUTION

Let, Laplace transform of $f(t) = \mathcal{L}\{f(t)\} = F(s)$

Laplace transform of $x_1 = \mathcal{L}\{x_1\} = X_1(s)$

Laplace transform of $x_2 = \mathcal{L}\{x_2\} = X_2(s)$



The system has two nodes and they are mass M_1 and M_2 . The differential equations governing the system are the force balance equations at these nodes. The free body diagram of mass M_1 is shown in fig 2. The opposing forces are marked as f_{m1} , f_{b1} , f_{b12} and f_{k1} .

$$f_{m1}\!=\!M_1\frac{d^2x_1}{dt^2} \hspace{0.2cm} ; \hspace{0.2cm} f_{b1}\!=\!B_1\frac{dx_1}{dt} \hspace{0.2cm} ; \hspace{0.2cm} f_{b12}\!=\!B_{12}\frac{d}{dt}(x_1\!-\!x_2) \hspace{0.2cm} ; \hspace{0.2cm} f_{k1}\!=\!K_1x_1$$

By Newton's second law, $\boldsymbol{f}_{\text{m1}} + \boldsymbol{f}_{\text{b1}} + \boldsymbol{f}_{\text{b12}} + \boldsymbol{f}_{\text{k1}} = \boldsymbol{f(t)}$

$$M_1 \frac{d^2 x_1}{dt^2} + B_1 \frac{d x_1}{dt} + B_{12} \frac{d (x_1 - x_2)}{dt} + K_1 x_1 = f(t)$$

On taking Laplace transform of above equation with zero initial conditions we get,

$$\begin{aligned} &M_{1}s^{2}X_{1}(s) + B_{1}sX_{1}(s) + B_{12}s[X_{1}(s) - X_{2}(s)] + K_{1}X_{1}(s) = F(s) \\ &X_{1}(s)[M_{1}s^{2} + (B_{1} + B_{12})s + K_{1}] - B_{12}sX_{2}(s) = F(s) \end{aligned}$$
(1)

The free body diagram of mass M_2 is shown in fig 3. The opposing forces are marked as f_{m2} , f_{b2} , f_{b12} and f_{k2} .

$$f_{m2} = M_2 \frac{d^2 x_2}{dt^2}$$
 ; $f_{b2} = B_2 \frac{dx_2}{dt}$

$$f_{b12} = B_{12} \frac{d}{dt} (x_2 - x_1)$$
; $f_{k2} = K_2 x_2$

By Newton's second law, $f_{m2} + f_{b2} + f_{b12} + f_{k2} = 0$

$$M_2 \frac{d^2 x_2}{dt^2} + B_2 \frac{dx_2}{dt} + B_{12} \frac{d(x_2 - x_1)}{dt} + K_2 x_2 = 0$$
(2)



$$M_2 \frac{d^2 x_2}{dt^2} + B_2 \frac{d x_2}{dt} + B_{12} \frac{d (x_2 - x_1)}{dt} + K_2 x_2 = 0 \qquad(2)$$

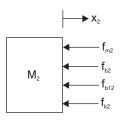


Fig 3.

$$\boldsymbol{M}_{2}s^{2}\boldsymbol{X}_{2}(s) + \boldsymbol{B}_{2}s\boldsymbol{X}_{2}(s) + \boldsymbol{B}_{12}s[\boldsymbol{X}_{2}(s) - \boldsymbol{X}_{1}(s)] + \boldsymbol{K}_{2}\boldsymbol{X}_{2}(s) = 0$$

$$X_2(s)[M_2s^2 + (B_2 + B_{12})s + K_2] - B_{12}sX_1(s) = 0$$

$$X_2(s)[M_2s^2 + (B_2 + B_{12})s + K_2] = B_{12}sX_1(s)$$

$$X_{2}(s) = \frac{B_{12}sX_{1}(s)}{[M_{2}s^{2} + (B_{2} + B_{12})s + K_{2}]}$$
.....(3)

Substituting for X₂(s) from equation (3) in equation (1) we get,

$$X_1(s) [M_1 s^2 + (B_1 + B_{12}) s + K_1] - \frac{(B_{12} s)^2 X_1(s)}{M_2 s^2 + (B_2 + B_{12}) s + K_2} = F(s)$$

$$\frac{X_{1}(s) \left[\, [M_{1}s^{2} + (B_{1} + B_{12})s + K_{1}] \, [M_{2}s^{2} + (B_{2} + B_{12})s + K_{2}] - (B_{12}s)^{2} \, \right]}{M_{2}s^{2} + (B_{2} + B_{12})s + K_{2}} = F(s)$$

$$\therefore \ \frac{X_1(s)}{F(s)} = \frac{M_2s^2 + (B_2 + B_{12})s + K_2}{[M_1s^2 + (B_1 + B_{12})s + K_1][M_2s^2 + (B_2 + B_{12})s + K_2] - (B_{12}s)^2}$$

From equation (3) we get,

$$X_{1}(s) = \frac{[M_{2}s^{2} + (B_{2} + B_{12})s + K_{2}]X_{2}(s)}{B_{12}s} \qquad(4)$$

Substituting for $X_1(s)$ from equation (4) in equation (1) we get,

$$\frac{X_2(s)[M_2s^2 + (B_2 + B_{12})s + K_2]}{B_{12}s}[M_1s^2 + (B_1 + B_{12})s + K_1] - B_{12}sX_2(s) = F(s)$$

$$X_2(s)\Bigg[\frac{[M_2s^2+(B_2+B_{12})s+K_2][M_1s^2+(B_1+B_{12})s+K_1]-(B_{12}s)^2}{B_{12}s}\Bigg] \ = \ F(s)$$

$$\therefore \ \frac{X_2(s)}{F(s)} = \frac{B_{12}s}{[M_2s^2 + (B_2 + B_{12})s + K_2][M_1s^2 + (B_1 + B_{12})s + K_1] - (B_{12}s)^2}$$

RESULT

The differential equations governing the system are,

1.
$$M_1 \frac{d^2 x_1}{dt^2} + B_1 \frac{dx_1}{dt} + B_{12} \frac{d(x_1 - x_2)}{dt} + K_1 x_1 = f(t)$$

$$2.\ M_2 \frac{d^2 x_2}{dt^2} + B_2 \frac{d x_2}{dt} + B_{12} \frac{d (x_2 - x_1)}{dt} + K_2 x_2 = 0$$

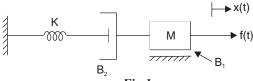
The transfer functions of the system are,

$$1. \ \, \frac{X_1(s)}{F(s)} = \frac{M_2 s^2 + (B_2 + B_{12}) s + K_2}{[M_1 s^2 + (B_1 + B_{12}) s + K_1][M_2 s^2 + (B_2 + B_{12}) s + K_2] - (B_{12} s)^2}$$

2.
$$\frac{X_2(s)}{F(s)} = \frac{B_{12}s}{[M_2s^2 + (B_2 + B_{12})s + K_2][M_1s^2 + (B_1 + B_{12})s + K_1] - (B_{12}s)^2}$$

EXAMPLE 1.4

Write the equations of motion in s-domain for the system shown in fig 1. Determine the transfer function of the system.



SOLUTION

Let, Laplace transform of $x(t) = \mathcal{L}\{x(t)\} = X(s)$

Laplace transform of $f(t) = \mathcal{L}\{f(t)\} = F(s)$

Let x_1 be the displacement at the meeting point of spring and dashpot. Laplace transform of x_1 is $X_1(s)$.

The system has two nodes and they are mass M and the meeting point of spring and dashpot. The differential equations governing the system are the force balance equations at these nodes. The equations of motion in the s-domain are obtained by taking Laplace transform of the differential equations.

The free body diagram of mass M is shown in fig 2. The opposing forces are marked as f_m, f_{h1} and f_{h2}.

$$f_m = M \frac{d^2 x}{dt^2}$$
 ; $f_{b1} = B_1 \frac{dx}{dt}$; $f_{b2} = B_2 \frac{d}{dt} (x - x_1)$

By Newton's second law the force balance equation is,

$$f_{m} + f_{b1} + f_{b2} = f(t)$$

$$\therefore M\frac{d^2x}{dt^2} + B_1\frac{dx}{dt} + B_2\frac{d}{dt}(x - x_1) = f(t)$$

On taking Laplace transform of the above equation we get,

$$Ms^2X(s) + B_1(s)X(s) + B_2 s[X(s) - X_1(s)] = F(s)$$

$$[Ms^2 + (B_1 + B_2)s] X(s) - B_2 sX_1(s) = F(s)$$

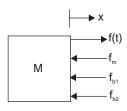


Fig 2.

....(1)

....(2)

The free body diagram at the meeting point of spring and dashpot is shown in fig 3. The opposing forces are marked as f_k and f_{ho} .

$$f_{b2} = B_2 \frac{d}{dt} (x_1 - x)$$
; $f_k = Kx_1$

By Newton's second law, $f_{h2} + f_k = 0$

$$\therefore B_2 \frac{d}{dt}(x_1 - x) + Kx_1 = 0$$

On taking Laplace transform of the above equation we get,

$$B_2s[X_1(s) - X(s)] + KX_1(s) = 0$$

$$(B_2s + K) X_1(s) - B_2 sX(s) = 0$$

$$\therefore X_1(s) = \frac{B_2 s}{B_2 s + K} X(s)$$

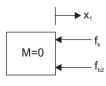


Fig 3.

Substituting for X₁(s) from equation (2) in equation (1) we get,

$$\begin{split} & \left[\, \mathsf{M} s^2 + (\mathsf{B}_1 + \mathsf{B}_2) \, s \, \right] \, \mathsf{X}(s) - \mathsf{B}_2 s \left[\, \frac{\mathsf{B}_2 s}{\mathsf{B}_2 s + \mathsf{K}} \, \right] \, \mathsf{X}(s) = \mathsf{F}(s) \\ & \mathsf{X}(s) \, \frac{\left[\, \mathsf{M} s^2 + (\mathsf{B}_1 + \mathsf{B}_2) \, s \, \right] (\mathsf{B}_2 s + \mathsf{K}) - (\mathsf{B}_2 s)^2 \right]}{\mathsf{B}_2 s + \mathsf{K}} = \mathsf{F}(s) \\ & \therefore \, \frac{\mathsf{X}(s)}{\mathsf{F}(s)} = \frac{\mathsf{B}_2 s + \mathsf{K}}{\left[\, \mathsf{M} s^2 + (\mathsf{B}_1 + \mathsf{B}_2) \, s \, \right] (\mathsf{B}_2 s + \mathsf{K}) - (\mathsf{B}_2 s)^2} \end{split}$$

RESULT

The differential equations governing the system are,

1.
$$M \frac{d^2x}{dt^2} + B_1 \frac{dx}{dt} + B_2 \frac{d}{dt} (x - x_1) = f(t)$$

2.
$$B_2 \frac{d}{dt} (x_1 - x) + K x_1 = 0$$

The equations of motion in s-domain are,

1.
$$[M s^2 + (B_1 + B_2)s] X(s) - B_2 sX_1(s) = F(s)$$

2.
$$(B_2s + K) X_1(s) - B_2 sX(s) = 0$$

The transfer function of the system is

$$\frac{X(s)}{F(s)} = \frac{B_2 s + K}{\left[M \, s^2 + (B_1 + B_2) s\right] \left(B_2 s + K\right) - \left(B_2 s\right)^2}$$

1.6 MECHANICAL ROTATIONAL SYSTEMS

The model of rotational mechanical systems can be obtained by using three elements, *moment* of inertia [J] of mass, dash-pot with rotational frictional coefficient [B] and torsional spring with stiffness [K].

The weight of the rotational mechanical system is represented by the moment of inertia of the mass. The moment of inertia of the system or body is considered to be concentrated at the centre of gravity of the body. The elastic deformation of the body can be represented by a spring (torsional spring). The friction existing in rotational mechanical system can be represented by the dash-pot. The dash-pot is a piston rotating inside a cylinder filled with viscous fluid.

When a torque is applied to a rotational mechanical system, it is opposed by opposing torques due to moment of inertia, friction and elasticity of the system. The torques acting on a rotational mechanical body are governed by *Newton's second law of motion* for rotational systems. It states that the sum of torques acting on a body is zero (or Newton's law states that the sum of applied torques is equal to the sum of opposing torques on a body).

LIST OF SYMBOLS USED IN MECHANICAL ROTATIONAL SYSTEM

 θ = Angular displacement, rad

 $\frac{d\theta}{dt}$ = Angular velocity, rad/sec

 $\frac{d^2\theta}{dt}$ = Angular acceleration, rad/sec²

T = Applied torque, N-m

 $J = Moment of inertia, Kg-m^2/rad$

B = Rotational frictional coefficient, N-m/(rad/sec)

K = Stiffness of the spring, N-m/rad